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Problem 2.24 (ASD)

D = 10 psf (assume girder self-weight is included in the 10 psf dead load)

$L_r = 20$ psf

S = 35 psf H = 0

R = 30 psf F = 0

W = 18 psf (acting downward) L = 0

E = 2 psf (acting downward) T = 0

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1 16-8: $D + F = 10$ psf

2 16-9: $D + H + F + L + T = 10$ psf

3 16-10: $D + H + F + (L_r \text{ or } S \text{ or } R) = 10 + 35 = 45$ psf

4 16-11: $D + H + F + 0.75(L + T) + 0.75(L_r \text{ or } S \text{ or } R) = 10 + 0.75(35) = 36.25$ psf

5 16-12: $D + H + F + (W \text{ or } 0.7E) = 10 + 18 = 28$ psf

6 16-13: $D + H + F + 0.75(W \text{ or } 0.7E) + 0.75L + 0.75(L_r \text{ or } S \text{ or } R)$
 $= 10 + 0.75(18 + 35) = 49.75$ psf

7 & 8 16-14 & 16-15: *not applicable since W and E act in same direction as D*

Maximum service load (for ASD) on the glulam girder is 49.75 psf based on ASCE 7 load combination 6 (IBC load combination 16-13).

[Note that one of the other service load combinations may be critical for design, depending on the applicable load duration factor, C_D . See discussion of C_D in Chapter 4 of the textbook.]

Problem 2.25 (LRFD)

Assume girder self-weight is included in the 10 psf dead load.

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1 16-1: $1.4(D + F) = 1.4(10) = 14$ psf

2 16-2: $1.2(D + F + T) + 1.6(L + H) + 0.5(L_r \text{ or } S \text{ or } R) = 1.2(10) + 0.5(35) = 29.5$ psf

3 16-3: $1.2D + 1.6(L_r \text{ or } S \text{ or } R) + (L \text{ or } 0.8W) = 1.2(10) + 1.6(35) + 0.8(18) = 82.4$ psf

4 16-4: $1.2D + 1.6W + L + 0.5(L_r \text{ or } S \text{ or } R) = 1.2(10) + 1.6(18) + 0.5(35) = 58.3$ psf

5 16-5: $1.2D + E + L + 0.2S = 1.2(10) + 2 + 0.2(35) = 21$ psf

6 & 7 16-6 & 16-7: *not applicable since W and E act in same direction as D*

Maximum factored load (for LRFD) on the glulam girder is 82.4 psf based on ASCE 7 load combination 3 (IBC load combination 16-3).

[Note that one of the other factored load combinations may be critical for design, depending on the applicable time effect factor, λ . See discussion of C_D and λ in Chapter 4 of the textbook.]



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